

Chapter 3 (conti.)

First Law of Thermodynamics
and Energy Equation

Work done at the moving boundary of a simple compressible system

- In a quasi-equilibrium process,

$$dW_b = FdL = PAdL = PdV$$

cf. non-equilibrium process: $dW = (p_{ext}A)dL = p_{ext}DV$

- ex) in a compression process,

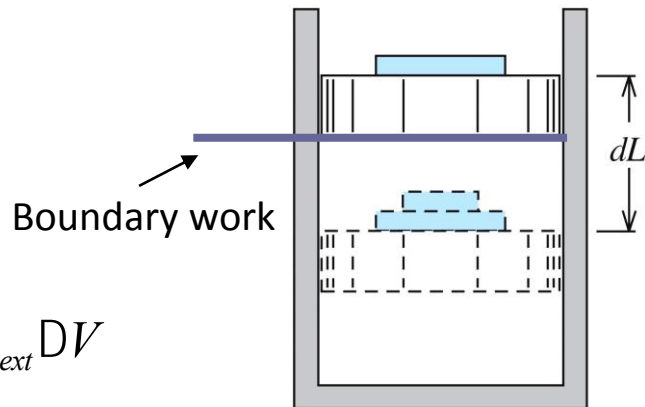


Figure 3.7
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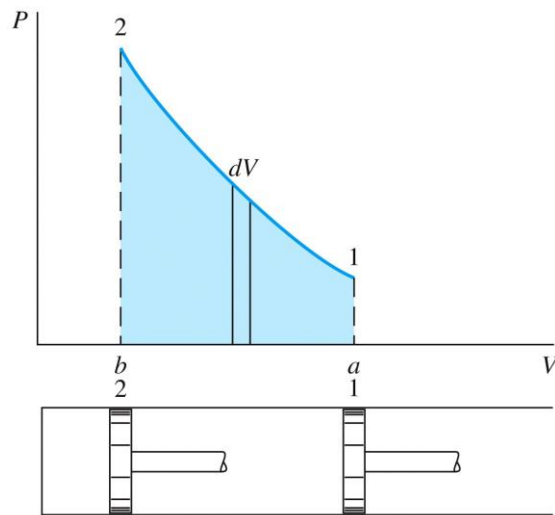


Figure 3.8
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$${}_1W_2 = \int_1^2 dW = \int_1^2 P dV$$

= the **area** of the shaded region under the P–V curve (a–1–2–b–a)

- As discussed earlier, work is a path function, and δW is an inexact differential. In other words, work is not a thermodynamic property

$${}_1W_2 = \int_1^2 dW \quad {}_1W_2 - W_1$$

$$\text{cf. } {}_1V_2 = \int_1^2 dV = V_2 - V_1$$

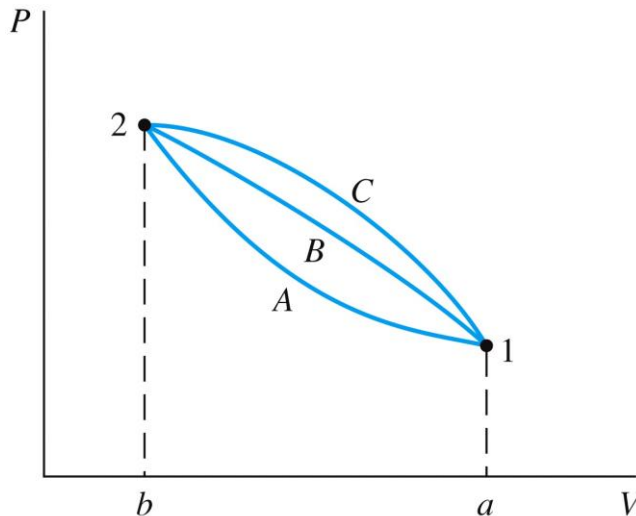


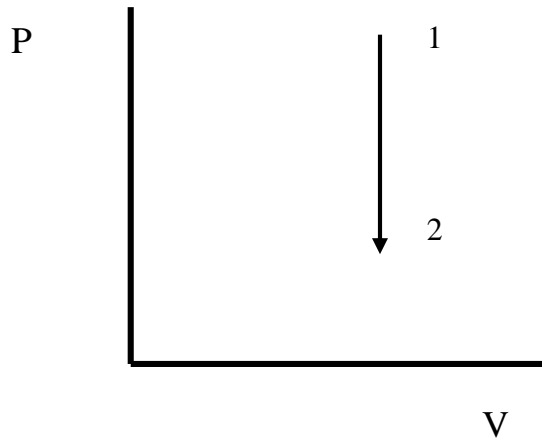
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The cyclic integral $\oint \delta W$ can be nonzero.

$$\text{cf. } \oint dV = 0$$

Work by the moving boundary in special cases

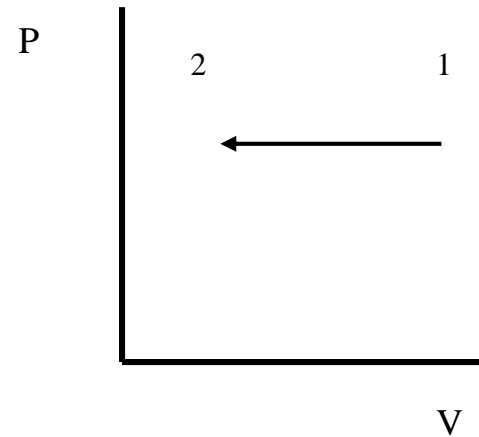
If the volume is held constant ($dV = 0$), then the boundary work equation becomes



P-V diagram for $V = \text{Constant}$

$$W_b = \int_1^2 P dV = 0$$

If the Pressure is held constant ($dP = 0$), then the boundary work equation becomes

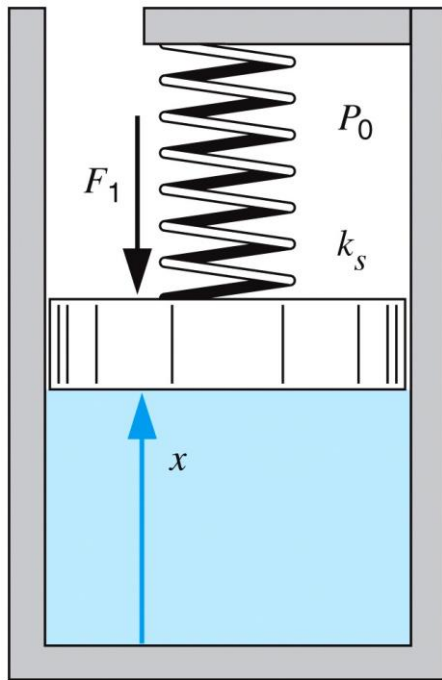


P-V diagram for $P = \text{Constant}$

$$\begin{aligned} W_b &= \int_1^2 P dV = P \int_1^2 dV \\ &= P(V_2 - V_1) \end{aligned}$$

Example 3.4

Consider a slightly different piston/cylinder arrangement, as shown in Fig. 3.10. In this example, the piston is loaded with a mass m_p the outside atmosphere P_o , a linear spring and a single point force F_1 . The piston traps the gas inside with a pressure P . A force balance on the piston in the direction of motion yields



$$m_p a = 0 = \dot{\uparrow} F_- - \dot{\downarrow} F_+$$

$$\dot{\downarrow} F_+ = \dot{\uparrow} F_-$$

$$\dot{\uparrow} F_- = PA$$

$$\dot{\uparrow} F_- = m_p g + P_o A + k_s (x - x_0) + F_1$$

$$P = \left\{ m_p g + P_o A + k_s (x - x_0) + F_1 \right\} / A$$

$$P = P_o + \frac{m_p g}{A} + \frac{F_1}{A} + \frac{k_s}{A^2} (V - V_0) = C_1 + C_2 V$$

slope

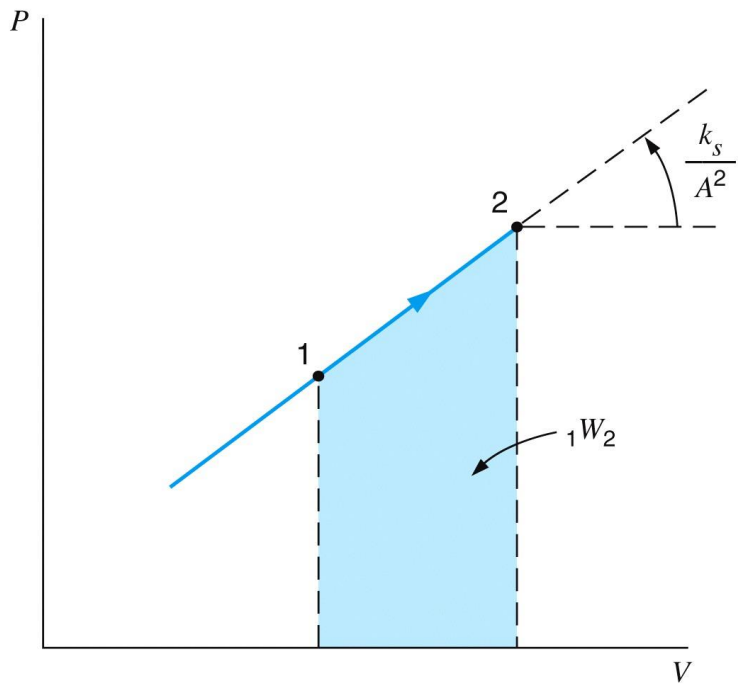


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$${}_1W_2 = \int_1^2 P dV = \frac{1}{2} (P_1 + P_2) (V_2 - V_1)$$

Polytropic process

$$PV^n = \text{const}$$

- The polytropic exponent n indicates the type of the process

Process	Exponent n
Constant pressure (or isobaric) process	0
Constant volume (or isochoric) process	$\pm\text{inf}$
Constant T (Isothermal) process of ideal gas	1

$$PV^n = \text{const}$$

$$P_1V_1^n = P_2V_2^n = \text{const}$$

$$P = \frac{\text{const}}{V^n} = \frac{P_1V_1^n}{V^n} = \frac{P_2V_2^n}{V^n}$$

Integration in a polytropic process

- When $n \neq 1$,

$$\begin{aligned} \int_1^2 P dV &= \text{const} \int_1^2 \frac{dV}{V^n} = \text{const} \left(\frac{V^{-n+1}}{-n+1} \right) \Big|_1^2 \\ &= \frac{\text{const}}{1-n} \left(V_2^{1-n} - V_1^{1-n} \right) = \frac{P_2 V_2^n V_2^{1-n} - P_1 V_1^n V_1^{1-n}}{1-n} \\ &= \frac{P_2 V_2 - P_1 V_1}{1-n} \Rightarrow \frac{mR(T_2 - T_1)}{1-n} \quad (\text{ideal gas}) \end{aligned}$$

- When $n = 1$,

$$\int_1^2 P dV = P_1 V_1 \int_1^2 \frac{dV}{V} = P_1 V_1 \ln \frac{V_2}{V_1}$$

Work in a Polytropic Process

Example 3.6

An ideal gas in a piston cylinder starts out with 200 kPa, 0.04 m³. Let us look at 4 different possible processes and find the work for each case.

Solution

a. Process: $P = C$, Heat the gas to $V_2 = 0.1 \text{ m}^3$

$$\begin{aligned} {}_1W_2 &= \int_1^2 P \, dV = P \int_1^2 dV = P (V_2 - V_1) \\ &= 200 \text{ kPa} \times (0.1 - 0.04) \text{ m}^3 = 12.0 \text{ kJ} \end{aligned}$$

b. Process: $T = C$, Heat the gas to $V_2 = 0.1 \text{ m}^3$

Ideal gas: $PV = mRT = C$ so polytropic with $n = 1$

$$\begin{aligned} {}_1W_2 &= \int_1^2 P \, dV = P_1 V_1 \ln \frac{V_2}{V_1} \\ &= 200 \text{ kPa} \times 0.04 \text{ m}^3 \times \ln \frac{0.1}{0.04} = 7.33 \text{ kJ} \end{aligned}$$

To do the process the mass (load) on piston varies

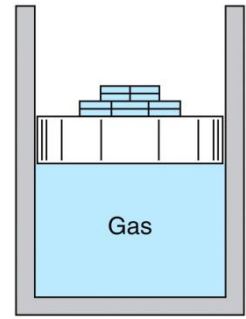


Figure 3.14
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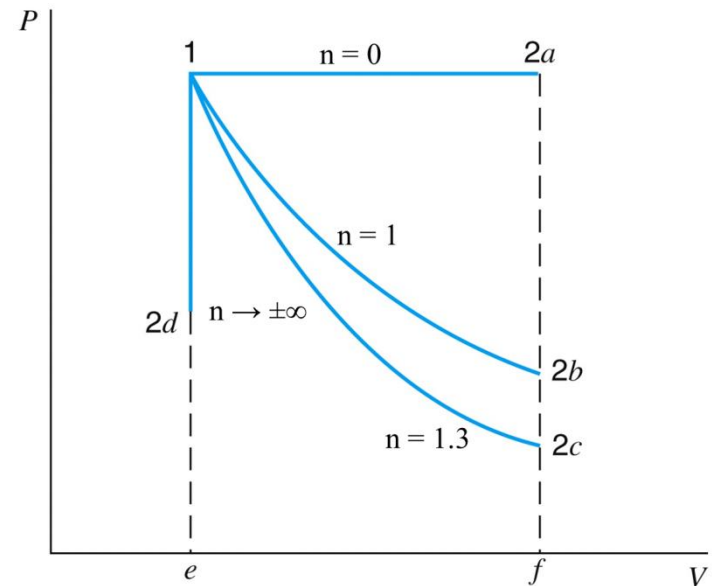


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Work in a Polytropic Process

Example 3.6 continued

c. Process: Polytropic with $n = 1.3$, Increase volume to $V_2 = 0.1 \text{ m}^3$

$$P_2 = P_1 (V_1 / V_2)^{1.3} = 200 \text{ kPa} \times (0.04 / 0.1)^{1.3} = 60.77 \text{ kPa}$$

$$\begin{aligned} {}_1W_2 &= \frac{1}{1-n} (P_2V_2 - P_1V_1) \\ &= \frac{1}{1-1.3} (60.77 \times 0.1 - 200 \times 0.04) \text{ kPa m}^3 \\ &= 6.41 \text{ kJ} \end{aligned}$$

d. Process: $V = C$, Cool the gas to $P_2 = 100 \text{ kPa}$

$${}_1W_2 = \int_1^2 P dV = 0$$

Comment:

To do the process (c) the mass (load) on piston varies

To do the process (d) the piston is locked in place

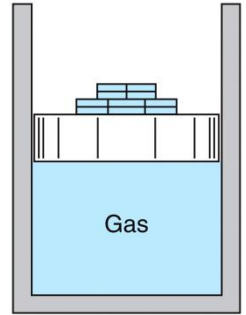


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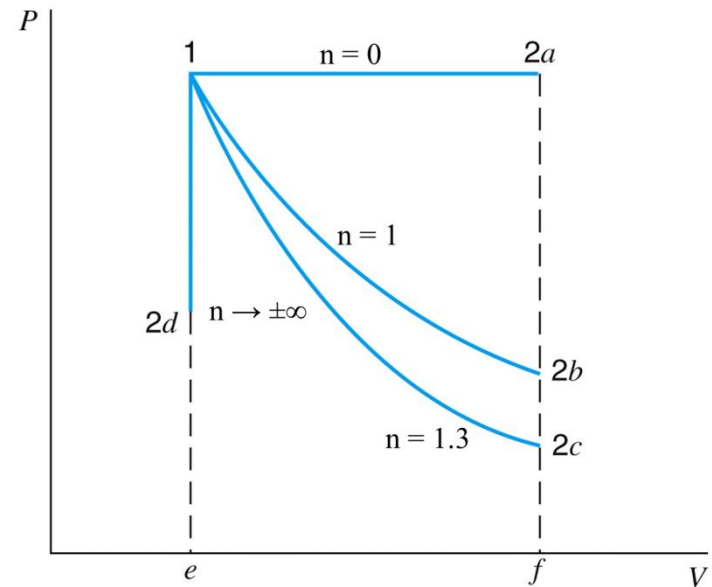


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Heat

- **Heat (Q)** is defined as the form of energy that is transferred across the boundary of a system at a given temperature to another system (or the surroundings) at a lower temperature by virtue of the temperature difference between the two system.

- ✓ Transient phenomenon (A body never contains heat.)
- ✓ A path function that has an inexact differential.

$$\int_1^2 dQ \neq Q_2 - Q_1$$

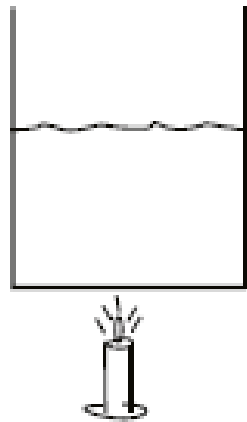
- ✓ Unit: joule, calorie (heat needed to raise 1 g of water from 14.5°C to 15.5°C, 1 cal = 4.2 J)
- **Adiabatic process** : a process with no heat transfer ($Q=0$)
- Specific heat transfer

$$q = \frac{Q}{m}$$

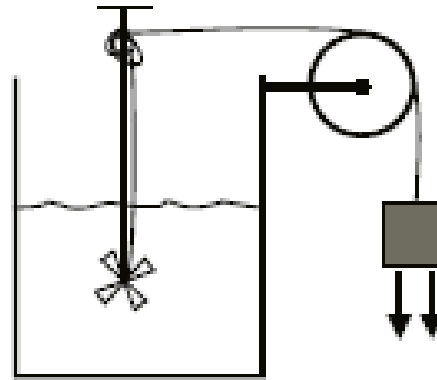
Equivalence of work and heat

Joule : it is possible to raise the temperature of H_2O

a) with only heat



b) with only work



Both transient phenomena
Both boundary phenomena
Both path function and inexact differential

Heat Transfer Modes

- **Conductive heat transfer**

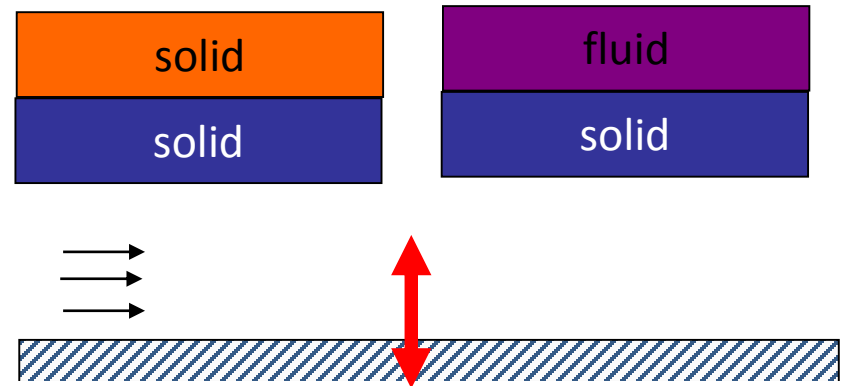
$$\dot{Q}_{cond} = -kA \frac{dT}{dx}$$

- **Convective heat transfer**

$$\dot{Q}_{conv} = hA\Delta T$$

- **Radiative heat transfer**

$$\dot{Q}_{rad} = \varepsilon A\sigma T^4$$



Internal Energy – a Thermodynamic Property

- U : internal energy (extensive property)
- $u = U/m$: specific internal energy (intensive property)
- **Internal energy** is a thermodynamic property that can substitute for an independent property of a pure substance. In the case of a pure substance, therefore, the internal energy can be obtained from two independent thermodynamic properties. (refer to table B.1.1 and B.1.2)
- In the steam tables, the internal energy values are obtained from calculation relative to a reference: zero for saturated liquid at the triple-point temperature.
- In the liquid-vapor saturation region,

$$U = U_{liq} + U_{vap}, \quad mu = m_{liq} u_f + m_{vap} u_g$$

$$u = (1 - x)u_f + xu_g$$

$$u = u_f + xu_{fg}$$



The Internal Energy

Example 3.8

Determine the missing property (P, T, v, x) for water at each of the following states:

- a. $T = 300^\circ\text{C}$, $u = 2780 \text{ kJ/kg}$; b. $P = 200 \text{ kPa}$, $u = 2000 \text{ kJ/kg}$

Solution

a) Table B.1.1 at 300°C : $u > u_g = 2563.0 \text{ kJ/kg}$, so superheated vapor,
x is undefined,

Table B.1.3 between 1600 and 1800 kPa at 300°C :

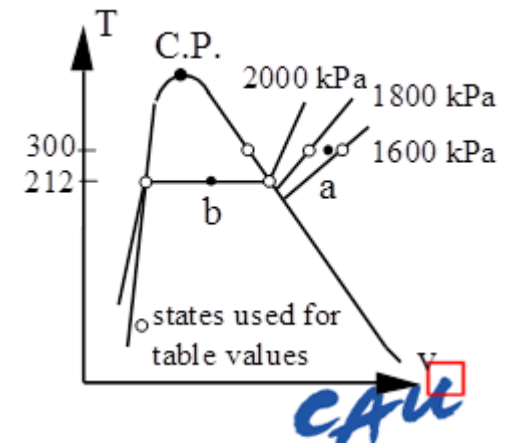
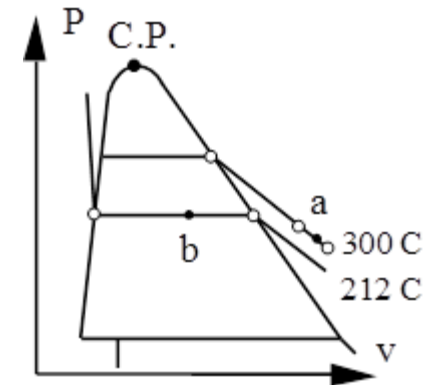
$$1600 \text{ kPa}, 300^\circ\text{C}: u = 2781.03 \text{ kJ/kg}; v = 0.15862 \text{ m}^3/\text{kg}$$

$$1800 \text{ kPa}, 300^\circ\text{C}: u = 2776.83 \text{ kJ/kg}; v = 0.14021 \text{ m}^3/\text{kg}$$

linear interpolation:

$$P = 1600 + 200 \frac{2780 - 2781.03}{2776.83 - 2781.03} = 1600 + 200 \times 0.24524 \\ = 1648 \text{ kPa}$$

$$v = 0.15862 + (0.14021 - 0.15862) \times 0.24524 = 0.1542 \text{ m}^3/\text{kg}$$



The Internal Energy

Example 3.8 continued

Determine the missing property (P, T, v, x) for water at each of the following states:

- a. $T = 300^\circ\text{C}$, $u = 2780 \text{ kJ/kg}$; b. $P = 200 \text{ kPa}$, $u = 2000 \text{ kJ/kg}$

Solution

b) Table B.1.2 at 2000 kPa:

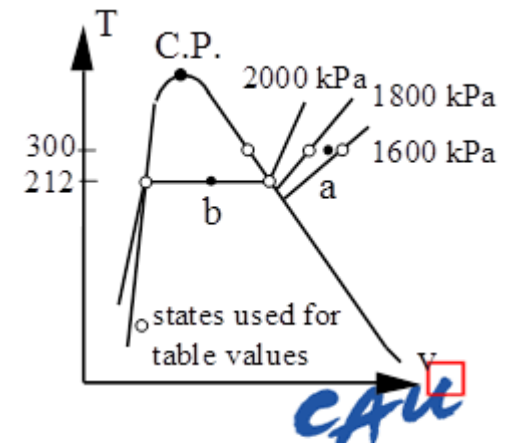
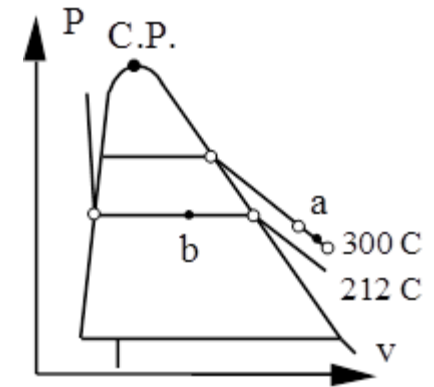
$$u_f = 906.4 < u < u_g = 2600.3 \text{ kJ/kg} \Rightarrow \text{two-phase}$$

$$u = 2000 = u_f + x u_{fg} = 906.4 + x \times 1693.8$$

$$\Rightarrow x = 0.6456$$

$$v = v_f + x v_{fg} = 0.001177 + 0.6456 \times 0.09845$$

$$= \mathbf{0.06474 \text{ m}^3/\text{kg}}$$



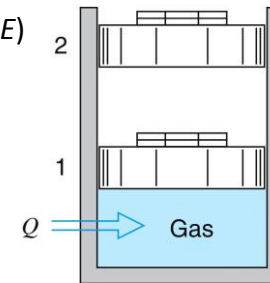
Enthalpy – a Thermodynamic Property

- $H \equiv U + PV$ (extensive property)
- $h = H/m = u + pv$: specific enthalpy (intensive property)
- For volumetric expansion of a gas in a *constant-pressure* quasi-equilibrium process, $\delta Q = dU + \delta W$ (Negligible *KE* & *PE*)

$$\delta Q = dU + PdV$$

$$\delta Q = d(U + PV) = dH$$

$${}_1Q_2 = H_2 - H_1$$



- In the steam tables, the enthalpy values are obtained from calculation relative to a reference.
- In the liquid-vapor saturation region,

$$H = H_{liq} + H_{vap} , \quad mh = m_{liq} h_f + m_{vap} h_g$$

$$h = (1 - x)h_f + xh_g$$

$$h = h_f + xh_{fg}$$